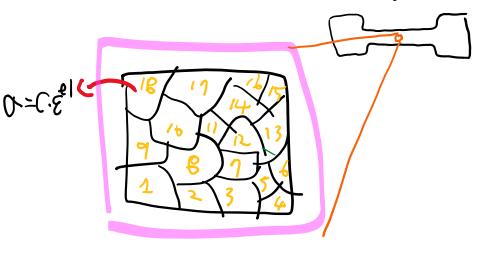
## Self-consistent scheme

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# The entire response/stimulus and individual response/stimulus?



Flyumptions

\* We know moduli/compliance of each grain

\* And let's assume they are "unitorm"

\* Each member hay "unitorm" weight\*

\*These are not "REGNIRED", but will make out analyses simple.

#### Two extreme cases

1. 
$$\overline{C}^{el} = \langle C^{el} \rangle = \langle (M^{el})^{-1} \rangle$$

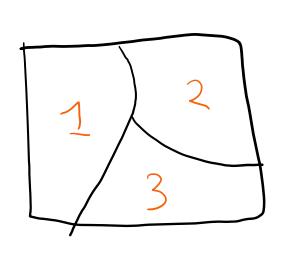
Thus,  $\overline{M}^{el} = (\overline{C}^{el})^{-1}$ ; invence

2.  $\overline{M}^{el} = \langle M^{el} \rangle$ 

Thus,  $\overline{C}^{el} = (\overline{M}^{el})^{-1} = (M^{el})^{-1}$ 

\* The above two cases may head to "equivalent" results or NOT!

## Let's use aggregate with only 3 members.



$$w^{2} = \frac{1}{3}$$
 $w^{3} = \frac{1}{3}$ 

x Each member has the same weights.

Although our overly simplified, can be applied to agghegate man seem things we'll loann from it there aggregates with many more members. Theregase with non equal weights

## Isotropic members but with tensors

$$R: M \in A = \begin{bmatrix} (0745^{\circ} - 51045^{\circ}) & -51045^{\circ} \\ 51045^{\circ} & -51045^{\circ} \end{bmatrix} = \sqrt{2} \begin{bmatrix} 1 & -1 \\ 1 & 1 \end{bmatrix}$$

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## Isotropic members

When the same weights.

When the same weights.

When the same weights.

When the same weights.

$$0 = 0^{\circ}$$
, 45°, 90°  $0 = 0^{\circ}$ 

$$C_{ij}^{el} = \begin{bmatrix} 200 & 0 \\ 0 & 200 \end{bmatrix} C_{ij}^{el}$$

W61, = Kikbiac ka

member 1.

$$C_{ij}^{el,'} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 200 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 200 & 0 & 0 & 0 \\ 0 & 200$$

 $C_{ij}^{0l,i} = \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} 200 & 0 \end{bmatrix} \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} \begin{bmatrix} 0 & -200 \\ 200 & 0 \end{bmatrix} \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} = \begin{bmatrix} 200 & 0 \\ 0 & 210 \end{bmatrix} \begin{bmatrix} 700 & 1 \\ 0 & 210 \end{bmatrix}$ 

Is supply was assumed for each stain

The supply property does not depend on

coordinate system.

Then if grains with different overtaken,

if grains with anthout overther it eventually reduces the case of "uniform" grain property.

19 Thur, the two extreme care's would

R: ME a = [ (07 45° -5145° ] = NI [ ] Celi = RikRje Cel member 3 R: Inta = [ (0) 90° - 5'in 90°] = [ 0 - 1]

Mei; = Kikbie Cel

While the same weights.

Where 
$$C_{ij} = C_{ij}$$

Where  $C_{ij} = C_{ij}$ 

Where  $C_{ij} = C_{i$ 

$$C_{ij}^{el} = \begin{bmatrix} 200 & 0 \\ 0 & 100 \end{bmatrix} Ga$$

Note transformation Rule.

$$R_i = R_i$$
 $E_i^{e_i} = R_i$ 
 $E_i^{e_i} = R_i$ 
 $E_i^{e_i} = R_i$ 
 $E_i^{e_i} = R_i$ 

W61, = Kikbir C61

$$C_{ij}^{0l,i} = \begin{bmatrix} 0 & -1 \end{bmatrix} \begin{bmatrix} 200 & 0 \end{bmatrix} \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & -10 \end{bmatrix} \begin{bmatrix} 0 & 10 \end{bmatrix} \begin{bmatrix} 0 & 10 \end{bmatrix} \begin{bmatrix} 0 & 10 \end{bmatrix} \begin{bmatrix} 10 & 0 \end{bmatrix} \begin{bmatrix} 1$$

We are young to explore two option to obtain tel by estimating the supliance of aggregate Mel Wing  $\overline{\mathcal{M}}^{\varrho} = \left( \frac{c}{c} \right)^{-1} = \left( \frac{c}{c} \right)^{-1}$ of ():Weight  $M_{el} = \langle M_{el} \rangle = \langle (c_{el})_{el} \rangle$ 

$$w^{2} = \frac{1}{3}$$

$$w^{2} = \frac{1}{3}$$

$$w^{3} = \frac{1}{3}$$

Note transformation Rule.  $0 = R_i \sigma_j$   $e^{e_i} = R_i e^{e_i}$   $e^{e_i} = R_{ik} R_{ik} e^{e_i}$ 

W61, = Kikbit C61

Exhame case 1
$$C_{11}^{el} = \langle C_{11}^{el} \rangle = \begin{bmatrix} 200 & 0 \\ 0 & 100 \end{bmatrix}_{3}^{2} + \begin{bmatrix} 150 & 50 \\ 50 & 150 \end{bmatrix}_{3}^{2} + \begin{bmatrix} 100 & 0 \\ 0 & 200 \end{bmatrix}_{3}^{2}$$

$$= \begin{bmatrix} 450 & 50 \\ 50 & 450 \end{bmatrix}_{3}^{2} - \begin{bmatrix} 9 & 1 \\ 1 & 9 \end{bmatrix}_{3}^{50}$$

$$= \begin{bmatrix} 450 & 50 \\ 50 & 450 \end{bmatrix}_{3}^{2} - \begin{bmatrix} 9 & 1 \\ 1 & 9 \end{bmatrix}_{3}^{50}$$

$$= \begin{bmatrix} 9 & 1 \\ 1 & 9 \end{bmatrix}_{3}^{2} - \begin{bmatrix} 9 & -1 \\ 1 & 9 \end{bmatrix}_{3}^{2} - \begin{bmatrix} 9 & -1 \\ 1 & 9 \end{bmatrix}_{400}^{2} - \begin{bmatrix} 9 & 1 \\ -1 & 9 \end{bmatrix}_{400}^{2} - \begin{bmatrix} 9 & 1 \\ -1 & 9 \end{bmatrix}_{4000}^{2} - \begin{bmatrix} 9 & 1 \\ -1 & 9$$

Now, unlike other previous analyses, the two ethreme cases studied led to two distinctive results.

cases studied led to two distinctive results.

$$\int M^{el} = \lim_{n \to \infty} \left[ \frac{4.15}{4.15} \right] \quad \text{case 1} \quad \text{form in } \quad \text{(APA)}$$

$$\int M^{el} = \frac{1}{100} \left[ \frac{9/2}{1/2} \right] \quad \text{case 2}$$

If the aggregate is loaded as much as  $\overline{O} = \begin{bmatrix} 100 \text{ M/a} \\ 200 \text{ M/a} \end{bmatrix}$  what is  $\overline{\xi}^{el} = \begin{bmatrix} ? \\ ? \end{bmatrix}$ Case 1  $\begin{bmatrix} 1 \\ 100 \end{bmatrix} = \begin{bmatrix} 0.75 \\ -0.75 \end{bmatrix} \begin{bmatrix} 1 \\ 200 \end{bmatrix} = \begin{bmatrix} 6.75 \\ -0.75 \end{bmatrix} \begin{bmatrix} 1 \\ -0.75 \end{bmatrix} \begin{bmatrix} 1$ 

$$(0) = \frac{1}{100} \begin{bmatrix} \frac{9}{12} - \frac{1}{12} \\ -\frac{1}{12} - \frac{1}{12} \end{bmatrix} \begin{bmatrix} \frac{100}{12} - \frac{100}{12} \\ -\frac{1}{12} - \frac{1}{12} \end{bmatrix} \begin{bmatrix} \frac{100}{12} - \frac{1}{12} \\ -\frac{1}{12} - \frac{1}{12} - \frac{1}{12} \end{bmatrix} \begin{bmatrix} \frac{1}{12} - \frac{1}{12} - \frac{1}{12} \\ -\frac{1}{12} - \frac{1}{12} - \frac{1}{12} - \frac{1}{12} - \frac{1}{12} \end{bmatrix} \begin{bmatrix} \frac{1}{12} - \frac{1}{12} - \frac{1}{12} \\ -\frac{1}{12} - \frac{1}{12} - \frac{1}{$$

Summan. \* Care 1 y led to two difficent \* care 2 | Ferults of Eel  $((c^{e_1})^{-1})$   $\neq$   $((c^{e_1})^{-1})$ The Guertion mu is, then,

The Guertion mu is, then,

way of estimating

what is the correct way of estimating

-ell\_(=els-1)  $M_{6}(=(C_{61})_{-1})$ 

Mathematically, if le run "FIND" a way to estimate Mel by Mel, that means...  $\rightarrow$   $\tilde{M}^{el}$  as a function of  $(M^{el,1}, M^{el,2}, ..., M^{el,n})$  $\rightarrow M^{-2}$  as a function of  $(M^{el}, R^{l}, R^{l}, R^{l}, R^{l}, R^{l}, R^{l}, R^{l}, R^{l})$ Chystallographic texture JET LE Know such a function, its "INVERSE".

we would be able to make use of its "INVERSE".

Summay. grain property (here we focus Mel) - when is "anisotrpil" and the grains are not in the same orientation, generally,  $\langle W_{61} \rangle \neq \langle (C_{61})_{-1} \rangle$ -) We need "better" extinuation of overall

propuly of polycryttal

7 In what follows, we study a particular
method widely studied, and in literature.